

# Characterization and Modeling of Size Effect on the Performances of 0.10 $\mu\text{m}$ RF MOSFETs for SOC Applications

Yo-Sheng Lin<sup>†</sup>, Hsin-Yuan Tu, Hong-Wei Chiu, and Shey-Shi Lu, *Senior Member, IEEE*

<sup>†</sup>Department of Electrical Engineering, National Chi-Nan University, Puli, Taiwan, R.O.C.

Tel: 886-4-92910960 ext.4101, Fax: 886-4-92917810, Email : [stephenlin@ncnu.edu.tw](mailto:stephenlin@ncnu.edu.tw)

Department of Electrical Engineering, National Taiwan University, Taipei, Taiwan, R.O.C.

**Abstract** — In this paper, we demonstrate the size effect on the DC and RF performances of 0.10  $\mu\text{m}$  RF MOSFETs for SOC applications. Our results show that for RF MOSFETs, the input impedance can be represented by a series RC circuit at low frequencies and a “shifted” parallel RC circuit at high frequencies. In addition, the output impedance can be represented by a “shifted” series RC circuit at low frequencies and a “shifted” parallel RC circuit at high frequencies. The appearance of the kink phenomenon of scattering parameters  $S_{11}$  and  $S_{22}$  in a Smith chart is caused by this inherent ambivalent characteristic of the input and output impedances. It was found that an increase of device’s width (or  $g_m$ ) enhances the kink effect of  $S_{11}$  and  $S_{22}$ . The present study enables RF engineers to understand the behaviors of S-parameters more deeply, and hence are helpful for them to create a fully scalable CMOS model for SOC applications.

## I. Introduction

The kink phenomenon in scattering parameter  $S_{22}$  of RF MOSFETs/MESFETs and BJTs/HBTs, which has been explained quantitatively [1]–[2], can be seen frequently in the literature [3]–[4]. However, the kink phenomenon in scattering parameter  $S_{11}$  of RF MOSFETs or BJTs has never been reported. In this paper, the kink phenomenon in  $S_{11}$  of RF MOSFETs is reported and explained quantitatively for the first time. It was found that an increase of device’s width enhances the kink effect. The kink phenomenon of  $S_{11}$  of RF MOSFETs is explained by deriving the input impedance (or admittance) of a four-terminal MOSFET under the measurement conditions of S-parameters.

From the point of view of device physics, the appearance of the kink phenomenon of  $S_{11}$  and  $S_{22}$  has nothing to do with any non-ideal characteristics due to device defects or trapping of carriers. Actually, it results from the interaction of  $C_{gs}$ ,  $C_{gd}$ ,  $C_{ds}$ ,  $g_m$ ,  $C_{bs}$ ,  $C_{bd}$ ,  $g_{mb}$ , and  $R_b$ , etc. If any of the previous terms results in a decrease of  $r$  and increase of  $g$ , then the kink phenomenon will become more prominent. In this paper, devices fabricated by a 0.10  $\mu\text{m}$  RF CMOS technology was used to study the size effect (or  $g_m$ ) on the kink phenomenon of  $S_{11}$ .

## II. DC Characteristics of 0.10 $\mu\text{m}$ RF MOSFETs

Key layout parameters, and DC and RF performances at  $V_{DS}=V_{GS}=1.2\text{V}$  of nMOS devices A-E studied in this work are summarized in Table I. Note that the corresponding pMOS devices A’-E’ with the same sizes as the nMOS devices listed in Table I were also fabricated, but are not listed here. Devices A-D are typical 0.10  $\mu\text{m}$  RF nMOSFETs for low-power RF-IC applications, while device-E is typical 0.10  $\mu\text{m}$  low-leakage nMOSFET for low-power and high-speed SRAMs applications. The only difference in process between devices A-D and device-E is the dosage of channel implantation. As shown in Table I, the normalized DC characteristics of devices A-D are nearly the same, so only DC characteristics of device-D will be discussed in the following.

The measured DC characteristics of device-D are shown in Fig. 1(a)–(d). Fig. 1(a) shows typical  $I_{DS}-V_{DS}$  characteristics. Fig. 1(b) shows typical  $I_{off}-V_G$  characteristics under various reverse body biases ( $V_B$ ). Fig. 1(c) shows the measured  $I_{off}-V_B$  characteristics under various temperatures. For 250/150 pA/ $\mu\text{m}$  nominal off-state currents ( $I_{off,nom}$ ) @1.1V $_{CC}=1.32\text{V}$ , n/pMOS with excellent 580/235  $\mu\text{A}/\mu\text{m}$  nominal drive currents @ $V_{CC}=1.2\text{V}$  were achieved. In addition, if additional channel implantations are done, 15/10 pA/ $\mu\text{m}$   $I_{off,nom}$  @1.1V $_{CC}=1.32\text{V}$  for n/pMOS can be achieved. The corresponding driving currents @ $V_{CC}=1.2\text{V}$  were 430/175  $\mu\text{A}/\mu\text{m}$  for n/pMOS, as summarized in Table I. Fig. 1(d) shows the  $I_{off}$  components versus temperature characteristics. As can be seen, the  $I_{EDT}$  leakage current was kept to be under the 10% of  $I_{off,max}$  of device-E (50 pA/ $\mu\text{m}$ ) at room temperature in order to meet the stringent  $I_{off,nom}$  requirement of 15 pA/ $\mu\text{m}$ . This ensures the possibility of tuning device-D to device-E without the need to increase the oxide thickness.

## III. RF Performance of 0.10 $\mu\text{m}$ RF MOSFETs

The measured  $S_{11}$  and  $S_{22}$  characteristics of device A-D are shown in Fig. 2(a)–(d). Fig. 2(a) and 2(b) show the measured  $S_{11}$  and  $S_{22}$  characteristics in a Smith chart,

respectively. Fig. 2(c) and 2(d) show the measured  $|S_{11}|$  and  $|S_{22}|$  characteristics in a Bode plot, respectively.

Based on Fig. 2 and the summarized results of  $S_{11}$  and  $S_{22}$  in table I, we can conclude that the kink phenomenon in  $S_{11}$  of RF MOSFETs can be interpreted in terms of poles and zeros only when the device's gate-width is not too small. In addition, the kink phenomenon in  $S_{22}$  of RF MOSFETs can be interpreted in terms of poles and zeros only when the device's gate-width is within a middle range. As shown in Table I, the kink phenomenon in  $S_{22}$  of device-D cannot be interpreted in terms of poles and zeros because its corresponding  $R_{ds}$  is too small (close to 50Ω) due to large gate-width (see Fig. 2(b)), so there is no local minimum in the Bode plot of  $S_{22}$  (see Fig. 2(d)).

On the other hand, we can see that an increase of device's width enhances the kink effect of  $S_{11}$  and  $S_{22}$ . In addition, the kink-frequency first increases then decreases with the increase of gate width. These trends can be explained by the following derived input-impedances both at low frequencies and at high frequencies. At low frequencies, the input impedance can be simplified to a simple series RC circuit as follows:

$$Z_{in} \approx R_g + R_{gs} \cdot \left( \frac{C'_{gs}}{C'_{gs} + C_M} \right)^2 + R_M \cdot \left( \frac{C_M}{C'_{gs} + C_M} \right)^2 + \frac{1}{j\omega(C'_{gs} + C_M)}$$

$$\approx r_s + \frac{1}{j\omega C_s} \quad (1)$$

where  $R_M = [R_L(C'_{ds} + C'_{gd}) + R'_{gd}C'_{gd}]/C_M$ ,  $C_M = C'_{gd}(1 + g'_m R_L)$ , in which  $R_L = R_{ds} \parallel (R_d + Z_O)$ . In addition, at high frequencies, the input impedance can be simplified to a "shifted" parallel RC circuit as follows:

$$Z_{in} \approx R_g + \left\{ \frac{C'_{gd} + C'_{gs}R_L}{R_L(C'_{gd} + C'_{ds} + C'_{db}) + R'_{sub}C'_{db} + R'_{dg}C'_{gd}} + j\omega(C'_{gs} + C_p) \right\}^{-1}$$

$$\approx R_g + (g_p + j\omega C_p)^{-1} \quad (2)$$

where  $C_p = [R_L C'_{gd}(C'_{db} + C'_{ds}) + C'_{db}R'_{sub}C'_{gd}(1 + g'_m R_L)]/[R_L(C'_{gd} + C'_{db} + C'_{ds}) + (C'_{db}R'_{sub} + C'_{gd}R'_{dg})]$ .

Fig. 3(a) shows the adopted small-signal equivalent circuit model. Fig. 3 (b) shows the measured and modeled S-parameters of device-C. The extraction of parameters was based on the method introduced in Ref. [5]. Fig. 3(c) shows the current gain and MSG/MAG versus frequency characteristics of device-C. Very good  $f_T$  and  $f_{max}$  of 43 GHz and 33 GHz, respectively, were attained.

Fig. 4(a) shows  $P_{in}$  versus  $P_{out}$ ,  $G_p$  and PAE characteristics of devices B-D. Fig. 4(b) shows  $P_{out}$  versus PAE and  $G_p$  characteristics of devices B-D. Fig. 4(c) shows  $V_{GB}$  versus  $P_{out}$  characteristics under  $P_{in}=5$  dBm of

devices B-D. Fig. 4(d) shows the two-tone third-order intermodulation interception point OIP3 of device-D at 2.4 GHz and 5.2 GHz. As can be seen from Fig. 4(a)-(d), very good power performance has been achieved. In addition, no any anomaly was found. These results show the 0.11 μm CMOS technology is very suitable for power applications.

#### IV. Conclusions

The size effect on the performance of 0.10 μm RF MOSFETs, especially on the anomalous kinks observed in  $S_{11}$  and  $S_{22}$  have been analyzed. In conclusion, the "anomalous kink" is a "normal behave" of  $S_{11}$  and  $S_{22}$ . From the point of view of device physics, the appearance of the kink has nothing to do with any non-ideal characteristics due to device defects or trapping of carriers. Actually, it results from the interaction of  $C_{gs}$ ,  $C_{gd}$ ,  $C_{ds}$ ,  $g_m$ ,  $C_{bs}$ ,  $C_{bd}$ ,  $g_{mb}$ , and  $R_b$ , etc. If any of the previous terms results in a decrease of  $r$  and increase of  $g$ , then the kink phenomenon of  $S_{11}$  and  $S_{22}$  will become more prominent.

#### References

- [1] S. S. Lu, C. C. Meng, T. W. Chen and H. C. Chen, *IEEE Trans. on Microwave Theory and Techniques*, vol. 49, no. 2, pp. 406-409, Feb. 2001.
- [2] H. Y. Tu, Y. S. Lin, P. Y. Chen, and S. S. Lu, *IEEE Trans. on Electron Devices*, vol. 49, no. 10, pp.1831-1833, Oct. 2002.
- [3] Y. Aoki, and Y. Hirano, "High-Power GaAs FETs," *High Power GaAs FET Amplifiers*, p. 81, 1993
- [4] T. Takahashi, S. Sasa, A. Kawano, T. Iwai, and T. Fuji, *IEEE, IEDM, Tech. Dig.*, 1994, pp. 191-194.
- [5] F. X. Pengg, *2002 Radio Frequency Integrated Circuits Symposium*, pp. 355-358.

Table I. Key layout parameters, and DC and RF performances at  $V_{DS}=V_{GS}=1.2V$  of devices A-E studied in this work.

	Device-A	Device-B	Device-C	Device-D	Device-E
width (μm)	6	36	72	144	144
number of finger	1	6	18	18	18
gate length (μm)	0.1	0.1	0.1	0.1	0.1
$I_{ds\_nom}$ (μA/μm)	575	577	579	580	430
$V_{L\_nom}$ (V)	0.3	0.3	0.3	0.3	0.44
$I_{off\_nom}$ (pA/μm)	290	292	295	296	15
$I_{off\_max}$ (pA/μm)	1000	1000	1000	1000	50
kink freq. of $S_{11}$ (GHz)	12.2	24.6	21.8	19.4	NA
local minimum of $ S_{11} $ (GHz)	28.2	24.6	21.8	19.4	NA
kink freq. of $S_{22}$ (GHz)	12.8	17	13.8	10	NA
local minimum of $ S_{22} $ (GHz)	28.2	17	13.8	NA	NA
$f_T$ (GHz)	< 0.2	29	43	43	NA
$f_{max}$ (GHz)	5	31	33	33	NA

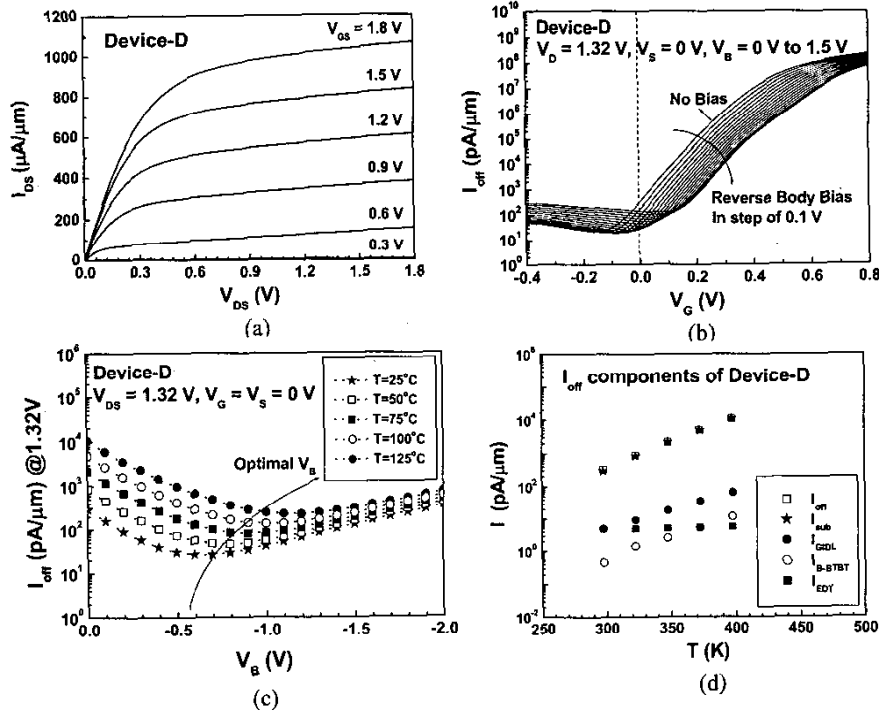


Fig. 1 The measured DC characteristics of device-D. (a)  $I_{DS}$  versus  $V_{DS}$  characteristics, (b)  $I_{off}$  versus  $V_G$  characteristics, (c)  $I_{off}$  versus reverse body bias characteristics under various temperatures, and (d)  $I_{off}$  components versus temperature characteristics.

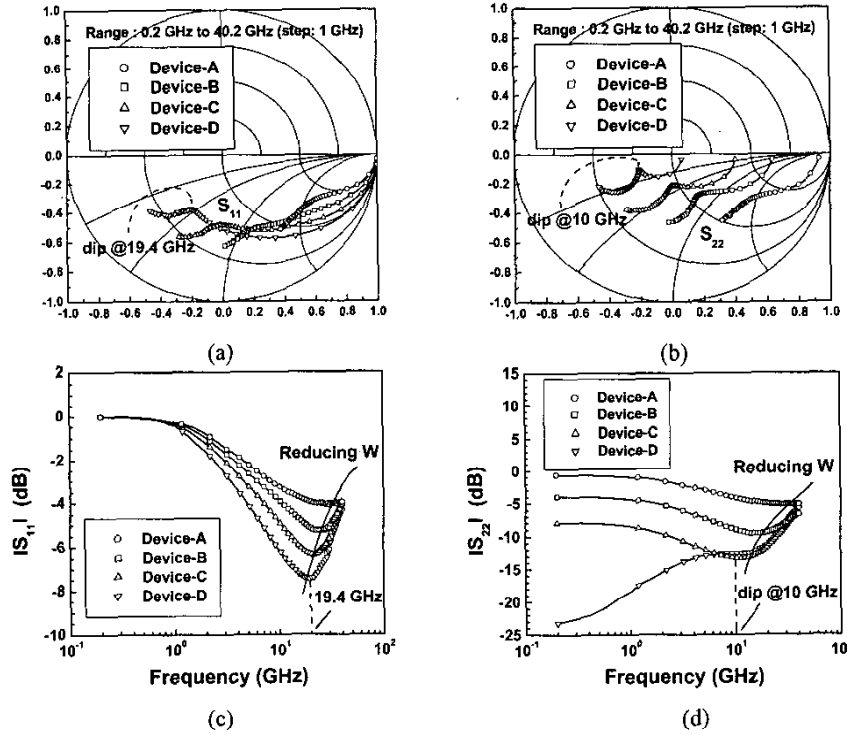


Fig. 2 (a) The measured  $S_{11}$  of devices A-D, (b) the measured  $S_{22}$  of devices A-D, (c)  $|S_{11}|$  versus frequency characteristics of devices A-D, and (d)  $|S_{22}|$  versus frequency characteristics of devices A-D.

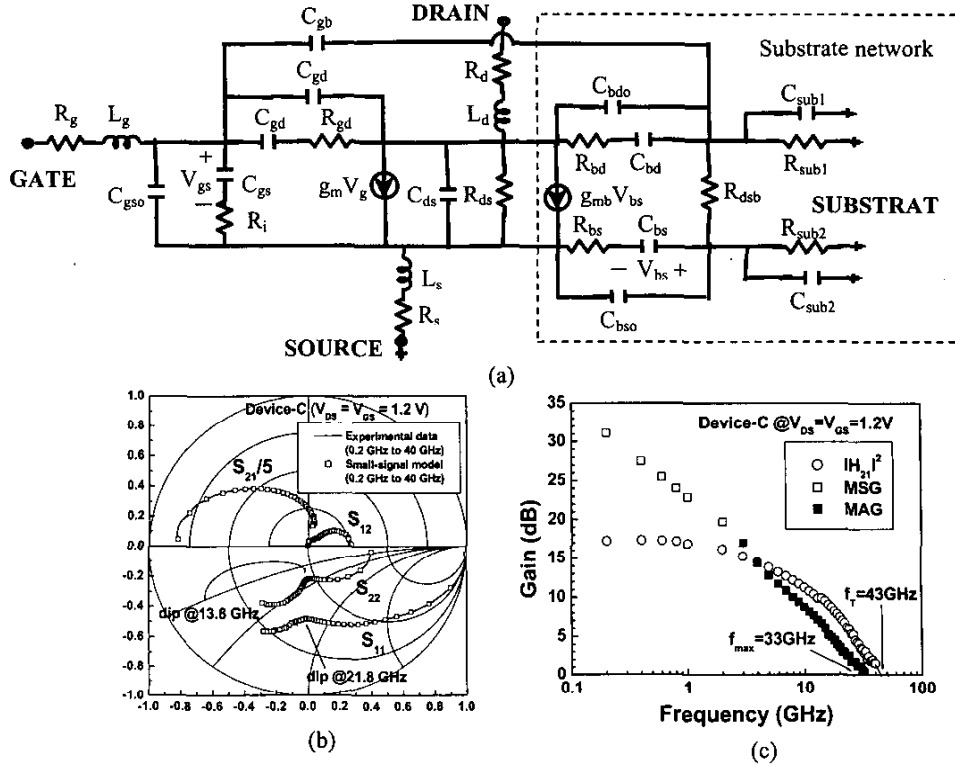


Fig. 3 (a) The adopted small-signal equivalent circuit model, (b) the measured and modeled S-parameters of device-C, and (c) the current gain and MSG/MAG versus frequency characteristics of device-D.

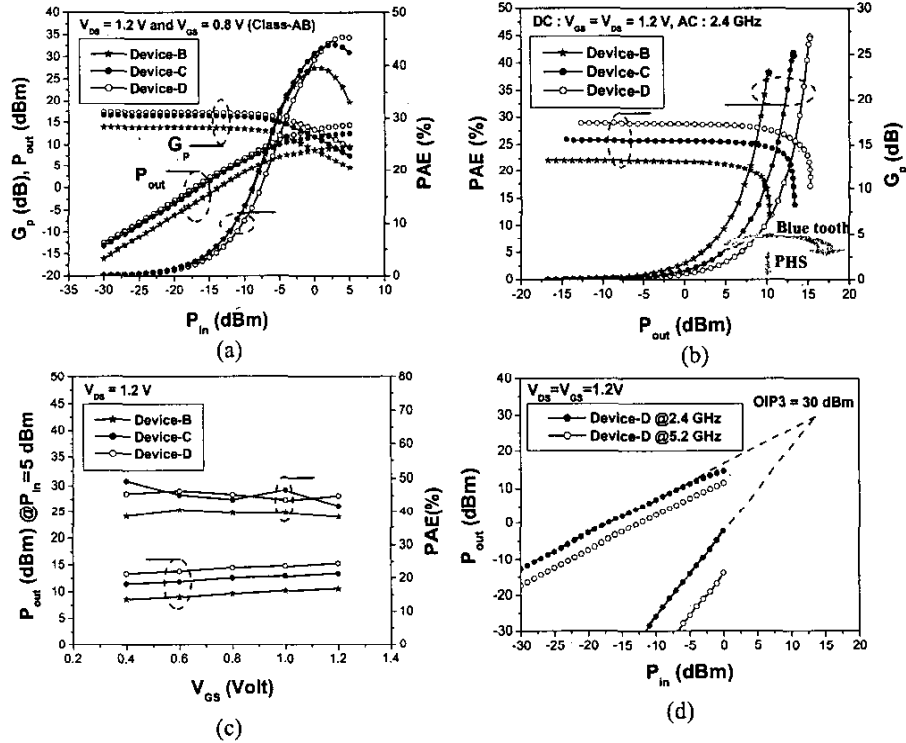


Fig. 4 (a)  $P_{in}$  versus  $P_{out}$ ,  $G_p$  and PAE characteristics of devices B-D, (b)  $P_{out}$  versus PAE and  $G_p$  characteristics of devices B-D, (c)  $V_{GB}$  versus  $P_{out}$  characteristics under  $P_{in} = 5$  dBm of devices B-D, and (d) two-tone third-order intermodulation interception point OIP3 of device-D at 2.4 GHz and 5.2 GHz.